Geo-electrical investigation of subsurface water resources in Kutunku, Gwagwalada Area Council, Abuja, Nigeria.

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Abstract: In this study, data obtained with the aid of an ABEM Terameter (SAS 300C), from twenty-five (25) Vertical Electrical Soundings (VES) stations in Kutunku, with maximum half-current electrodes spacing AB/2, of 170m and maximum half-potential electrodes spacing MN/2, of 7.5m for most of the profiles, were analysed with IPI2Win software. The analysis indicated 3 to 5 geo-electric layers where the former was predominant and the lithologic units were interpreted to consist of sandy top soil, clay/clayey sand, lateritic sand, compact laterite, weathered/fractured basement and fresh basement. Layer resistivity ranges were $1.95 - 1360\Omega m$, 0.4 - 1000 m, 0 $1723\Omega m$, 7.7 - $180000\Omega m$ and 71 - $44878\Omega m$ for the first, second, third and fourth layers respectively. In the same vein, layer depth ranged from 0.6 - 4.3m, 1.1 - 47.3m, 3.9 - 56.9m and 31.1m to undetermined depth. The second layer in most of the profiles showed conductive zones with low resistivity values ranging from $0.403\Omega m$ to $151\Omega m$. In most of the profiles, the third layer manifested as the last layer, predominantly with high resistivity readings of the order of $10^3 \Omega m$ to $10^5 \Omega m$ with unknown depths suspected to be fresh basement rocks. In the few profiles where four geo-electric layers were detected, with the exception of VES 18, the resistivity values (in Ωm), obtained for the last layer, were of the order of 10^3 and above, with unknown depth suspected to be fresh basement rocks. Amongst the second, third and fourth layers, the second layer mostly constitute the aquifer unit in the area with weathered/fractured basement rock type. The stations of highest groundwater potential were found to be VES 2, VES 5, VES 8, VES 14, VES 21, VES 24 and VES 25 because of the thicknesses of the layers interpreted as weathered or fractured zones which ranged from 25m to 55m. Keywords: Resistivity, Terameter, Kutunku, geo-electric layers, aquifer.

I. Introduction

Water is vital for life sustenance as it is deployed by man for several uses such as drinking, sanitation, cooking, industrial processing, hydropower generation, agriculture, fishery, ecosystem support. Water exists in different forms in the biosphere, atmosphere, lithosphere including ice cap, glaciers, ground surfaces and underground. However, surface and ground water sources are more readily available for abstraction if its quality is not compromised. According to Savenije and Van der Zaag (2002), Integrated Water Resource Management (IWRM) involves the consideration of all physical aspects of water resources including groundwater, at different temporal and spatial scales of the hydrological cycle and the related quality aspects. Unlike saline ocean or sea waters, groundwater is fresh, thus it is a finite resource (Van der Gaal and Savenije, 2011). According to a United Nations world water development report of 2003, groundwater is approximately 0.76% of water on earth. The same report indicates that it is about 30.1% of the world's freshwater resource. Groundwater can be found in both sedimentary and basement complex terrain.

In basement geology, groundwater occurs in weathered mantle, joints and fracture system in the unweathered rocks (Olorunfemi and Olorunniwo, 1985; Ako and Olorunfemi, 1989; Olayinka and Olorunfemi, 1992; Mallam and Emenike, 2008; Amadi et al., 2015) and it is most often localized (Adiat et al., 2009). The zones of possible high groundwater yield in basement terrain are strata often characterized by fractures, relatively low resistivity and thick overburden (Olorunfemi and Fasuyi, 1993). Thus, there is an encouraging trend of the use of geophysical studies prior to the drilling of boreholes for groundwater exploration (Mallam, 2004). Although the use of geotechnical and hydrogeological techniques, remote sensing, geographical information systems, and multicriteria analysis for delineating groundwater potential zones lack the precision of an in-situ analysis (Adiat et al., 2012; Madrucci et al., 2008), the electrical resistivity method is usually preferable because of the resistivity contrasts obtained when the groundwater zone is reached (Ishola et al., 2013). Electrical Resistivity method has become increasingly applied in groundwater prospecting in basement complex terrain (Olayinka and Olorunfemi, 1992; Olorunfemi et al., 1999; Omosuyi, 2000; Eduvie et al., 2003; Lateef, 2012; Okafor and Mamah, 2012; Dikedi, 2012; Abdulsalam and Ologe, 2013; Ishola et al., 2013; Odeyemi, 2014; Akinrinade and Olabode 2015; Amadi et al., 2015) and in sedimentary basin (De Beer and Blume, 1985; Mbonu et al., 1991; Emenike, 2000; Okolie et al., 2007; Oseji, 2009; Oseji and Ujuanbi, 2009; Oseji, 2010; Alile et al., 2011; Anomohanran, 2013). Apart from being non-invasive, the resistivity method is less expensive and time efficient when compared with test drilling and stratigraphy analysis which are other

ways of determining aquifer locations and characteristics (Todd, 1980; Fetter, 1994; Adiat *et al.*, 2013; Ishola *et al.*, 2013). In this paper, the groundwater potential and lithology in Kutunku is investigated using geo-electrical method. The result of the processed Vertical Electrical Sounding (VES) resistivity data and borehole lithology logs were integrated in order to assess the groundwater development prospect at the study area.

II. Physiography Of The Study Area

The study area is Kutunku in Gwagwalada Area Council, Federal Capital Territory (FCT), Nigeria. It lies within latitudes 8°55'00"N and 8°56'30"N, and between longitudes 7°03'30"E and 7°05'00"E. Gwagwalada is a suburb of the FCT, situated along Abuja-Lokoja road, about 55km South-west of Abuja City centre, between latitude 8°49' and 9°04' North and longitudes 6°50' and 7°06' East (Abuja Guide, 2002). According to a publication of the Nigerian Geological Survey Agency (2006), FCT lies within latitudes 8°22'N and 9°26'N and longitudes 6°42'E and 7°43'E.

The study area is within the tropical savannah vegetation zone. River Usuma and its tributaries drain the area. The map in figure 1 shows the topographic variation in elevation, VES stations and other physical features in the study area.



Figure 1: Location map of the study area.

III. Geology Of The Study Area

FCT is predominantly underlain by the Nigerian Basement Complex rock of the Precambrian age (Mamman and Oyebanji, 2000). Figure 2 shows the geologic map of FCT indicating the basic geologic formations. The rocks include different textures of granites, gneiss, migmatites, diorites, metasediments and pegmatites (Eduvie et al., 2003; Dikedi, 2012). Dikedi (2012) documented that the geology of the FCT is same as that of Gwagwalada. Groundwater is found mainly in the variable weathered/transition zone and in fractures, joints and cracks of the crystalline basement while sparse amount of water can be obtained in the freshly unweathered bedrock below the weathered layers (Eduvie et al., 2003).



IV. Materials And Method

An Abem Terameter SAS 300c, batteries, two pairs of electrodes, insulated multi-strand copper cables, non-conducting measuring tape, Megellan Triton 300 GPS (WP001) device, hammer and four crocodile clips were deployed to the field to aid in data acquisition.

The principle of operation of resistivity method depends on the fact that any subsurface variation in conductivity alters the form of current flow within the earth and this in turn affect the distribution of electric potential. Thus, it is possible to have information about the subsurface formations from potential measurements made at the surface. The microscopic form of ohm's law is the fundamental formula used in resistivity measurements. That is,

The Vertical Electrical Soundings (VES) were carried out using the Schlumberger electrode configuration described by Zohdy *et al.*, (1974). The arrangement of electrodes is illustrated in figure 3. L is half the distance between the current electrodes and L is half the spacing between the potential electrodes. The potential electrodes indicated by P_1 and P_2 are kept fixed and the current electrode separation is varied to obtain the changes in subsurface resistivity at greater depth. The field procedure was implemented by taking soundings with successive increase in the distance between current electrodes (AB) along the profile while the distance between potential electrodes (MN), was kept fixed. At the point when the measuring capability of the Terrameter tended to be overwhelmed as a result of a decreasing potential difference across MN, a new value for MN larger than the preceding value was taken and the survey was continued.



Figure 3: Diagram of Schlumberger array

The apparent resistivity equation for the Schlumberger array is given by

$$\rho_a = \pi \left(\frac{L^2}{2l} - \frac{2l}{4} \right) R$$
(2)

where, the geometric factor, G

$$G = \pi \left(\frac{L^2}{2l} - \frac{2l}{4} \right) \dots (3)$$

Vertical Electrical Soundings (with AB/2, ranging between 2m and 500m, and MN/2, ranging between 0.5m and 45.5m) were carried out at twenty-five VES stations and resistivity data were obtained. The coordinate locations and elevations above sea level were obtained with GPS device. Borehole lithology logs for two locations near the study area were obtained to aid in result interpretation.

V. Results And Discussion

The resistivity data were processed with IPI2Win software and the layer curve characteristics identified include H, HKH, HA, KH and HK-type. H-type curve characteristics was however predominant. Typical curve types are shown in figures 4a to 4e. The result of geo-electric parameters obtained is presented in table 1. Two borehole lithology logs as shown in figure 4f obtained near the area aided as geologic reference in the result interpretation.













Figure 4d: Layer curve and interpretation for VES 18.



Figure 4e: Layer curve and interpretation for VES 21.



Figure 4f: Borehole lithology logs obtained near the study area.

TABLE 1:	Summary	of the VES	interpr	etation result

VES No.	Curve Type	Layer	Resistivity (Ωm)	Thickness (m)	Overburden Thickness (m)	Lithological equivalence	Groundwater Potential
1	Н	lı	72.8	2.6	2.6	Sandy top soil	Very Low
		l_2	24.0	5.4	8.5	Clay/Clayey sand	
		l ₃	91750.0			Fresh basement	
2	Н	lı	553.9	0.6	0.6	Sandy top soil	Moderate
		l_2	77.9	30.5	31.1	Weathered/fractured	
						basement	
		l ₃	97325.0			Fresh basement	
3	Н	l_1	202.8	0.7	0.7	Sandy top soil	Poor
		l_2	37.6	18.9	19.7	Weathered/fractured	
						basement	
		l ₃	58133.0			Fresh basement	
4	Н	l_1	475.9	3.0	3.0	Sandy top soil	Poor
		l_2	33.4	9.2	12.2	Weathered/fractured	
						basement	
		l ₃	47501.0			Fresh basement	
5	Н	l1	396.3	2.2	2.2	Sandy top soil	Moderate
		l_2	56.9	45.1	47.3	Weathered/fractured]

						basement		
		l ₃	5692.0			Fresh basement		
6	Н	l ₁	288	1.44	1.44	Sandy top soil	Very Low	
		l ₂	10.3	4.08	5.52	Clay/Clayey sand	_	
		l ₃	17927			Fresh basement	X 7 X	
7	Н	ι ₁	1.95	0.719	0.719	Sandy top soil	Very Low	
		l ₂	0.403	1.31	2.03	Clay/Clayey sand		
0	UIVII	13	1729			Fresh basement	Madausta	
0	нкн	1	1300	3.34	5.34	Sandy top soll	Moderate	
		12	50.1	3.03	0.98	Composted laterite		
		13	1424	0.91	21.4	Wastbarad/Frasturad	_	
		14	/1.4	15.5	51.4	hasement		
		le.	81914			Eresh basement		
9	н	L,	477	1.01	1.01	Sandy top soil	Very Low	
Í		12	6.68	1.57	2.58	Clay/Clayey sand	Very Low	
		13	15125			Fresh basement		
10	Н	ե	244	2.58	2.58	Sandy top soil	Poor	
		l ₂	72.4	15.4	18	Weathered/fractured		
		2			-	basement		
		l_3	110000			Fresh basement		
11	Н	l1	456	4.34	4.34	Sandy top soil	Low	
		l_2	81.3	5.63	9.97	Weathered/fractured		
						basement		
		l3	180000			Fresh basement		
12	Н	l_1	72.4	1.38	1.38	Sandy top soil	Very Low	
		l_2	2.52	1.31	2.69	Clay/Clayey sand		
		l ₃	12167			Fresh basement		
13	Н	l_1	452	2.26	2.26	Sandy top soil	Poor	
		l_2	53.3	10.1	12.4	Weathered/fractured		
						basement		
		l3	36023			Fresh basement		
14	н	ι ₁	246	1.29	1.29	Sandy top soil	Moderate	
		l_2	62.3	25.6	26.9	Weathered/fractured		
		1	65752			Erech becoment		
15	ц	13	473			Sandy top soil	Door	
15	11	ι	475	1.4/	1.47	Sandy top son	1 001	
		1.	92.7	18.5	20	Weathered/fractured		
		l_2	92.7	18.5	20	Weathered/fractured basement		
		l ₂	92.7	18.5	20	Weathered/fractured basement Fresh basement	_	
16	Н	l ₂ l ₃ l ₁	92.7 120000 243	18.5 1.96	20 1.96	Weathered/fractured basement Fresh basement Sandy top soil	Low	
16	Н	l_2 l_3 l_1 l_2	92.7 120000 243 22.6	18.5 1.96 2.04	20 1.96 4.0	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement	Low	
16	Н	$ \begin{array}{c} l_2 \\ \hline l_3 \\ \hline l_1 \\ \hline l_2 \\ \hline l_3 \end{array} $	92.7 120000 243 22.6 806	18.5 1.96 2.04 	20 1.96 4.0 	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement	Low	
16	H	$\begin{array}{c} l_2\\ \hline l_3\\ \hline l_1\\ \hline l_2\\ \hline l_3\\ \hline l_1\end{array}$	92.7 120000 243 22.6 806 26.7	18.5 1.96 2.04 0.62	20 1.96 4.0 0.62	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil	Low	
16 17	H	l_2 l_3 l_1 l_2 l_3 l_1 l_2	92.7 120000 243 22.6 806 26.7 1723	18.5 1.96 2.04 0.62 0.45	20 1.96 4.0 0.62 1.07	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite	Low	
16 17	H	$\begin{array}{c} l_{2} \\ \hline l_{3} \\ \hline l_{1} \\ \hline l_{2} \\ \hline l_{3} \\ \hline l_{4} \\ \hline l_{2} \\ \hline l_{4} \\ \hline l_{2} \\ \hline l_{3} \\ \hline \end{array}$	92.7 120000 243 22.6 806 26.7 1723 25.2	18.5 1.96 2.04 0.62 0.45 3.93	20 1.96 4.0 0.62 1.07 5.0	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured	Low	
16 17	Н		92.7 120000 243 22.6 806 26.7 1723 25.2	18.5 1.96 2.04 0.62 0.45 3.93	20 1.96 4.0 0.62 1.07 5.0	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement	Low	
16 17	H	l ₂ l ₃ l ₁ l ₂ l ₃ l ₁ l ₂ l ₃ l ₃ l ₄	92.7 120000 243 22.6 806 26.7 1723 25.2 3312	18.5 1.96 2.04 0.62 0.45 3.93	20 1.96 4.0 0.62 1.07 5.0 	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement	Low	
16 17 18	H KH HK	l ₂ l ₃ l ₁ l ₂ l ₃ l ₁ l ₂ l ₃ l ₃ l ₄ l ₁	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249	18.5 1.96 2.04 0.62 0.45 3.93 1.08	20 1.96 4.0 0.62 1.07 5.0 1.08	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Sandy top soil	Low Low Low	
16 17 18	H KH HK	$\begin{array}{c} l_{2} \\ \hline l_{3} \\ l_{1} \\ l_{2} \\ \hline l_{3} \\ \hline l_{1} \\ \hline l_{2} \\ \hline l_{3} \\ \hline l_{4} \\ \hline l_{4} \\ \hline l_{4} \\ \hline l_{2} \\ \end{array}$	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249 9.71	18.5 1.96 2.04 0.62 0.45 3.93 1.08 0.84	20 1.96 4.0 0.62 1.07 5.0 1.08 1.92	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Fresh basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Sandy top soil Clay/Clayey sand	Low Low Low	
16 17 18	H KH HK	l2 l3 l1 l2 l3 l3 l4 l4 l4 l4 l4 l2 l3	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249 9.71 3060	18.5 1.96 2.04 0.62 0.45 3.93 1.08 0.84 2.88	20 1.96 4.0 0.62 1.07 5.0 1.08 1.92 4.8	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Fresh basement Sandy top soil Clay/Clayey sand Compacted laterite	Low Low Low	
16 17 18	H KH HK	l2 l3 l1 l2 l3 l3 l4 l4 l4 l2 l3 l3 l4	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249 9.71 3060 242	18.5 1.96 2.04 0.62 0.45 3.93 1.08 0.84 2.88	20 1.96 4.0 0.62 1.07 5.0 1.08 1.92 4.8 	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Fresh basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured Veathered/fractured	Low Low Low	
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16 17 18 19	H KH HK HK	l2 l3 l1 l2 l3 l4 l4 l4 l2 l3 l4 l4 l4 l4 l4 l4 l1 l2 l3 l3 l4 l4 l1 l2 l3 l3 l4 l1 l2 l3 l3 l1 l2 l3 l1 l2 l3 l3 l1 l1 l2 l3 l1 l1 l2 l3 l1 l2 l3 l3 l1 l3 l3 l1 l3 l3 l3 l3 l3 l3 l3 l3 l3 l3 l3 l3 l3	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249 9.71 3060 242 194 92.7	18.5 1.96 2.04 0.62 0.45 3.93 1.08 0.84 2.88 4.1	20 1.96 4.0 0.62 1.07 5.0 1.08 1.92 4.8 4.1 2.00	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured basement Sandy top soil Weathered/fractured basement Sandy top soil	Low Low Low Low	
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16 17 18 19	Н КН НК Н	l2 l3 l1 l2 l3 l4 l1 l2 l3 l1 l2 l3 l1 l2 l3	92.7 120000 243 22.6 806 26.7 1723 25.2 3312 249 9.71 3060 242 194 29.2 668 201	18.5 1.96 2.04 0.62 0.45 3.93 1.08 0.84 2.88 4.1 3.99 2.22	20 1.96 4.0 0.62 1.07 5.0 1.08 1.92 4.8 4.1 8.09 2.22	Weathered/fractured basement Fresh basement Sandy top soil Weathered/basement Fractured basement Sandy top soil Compacted laterite Weathered/fractured basement Fresh basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured basement Sandy top soil Clay/Clayey sand Compacted laterite Weathered/fractured basement Sandy top soil Weathered basement Fractured basement Fractured basement	Low Low Low Low	
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		l ₄	1834			Fresh basement	
24	HA	lı	190	1.38	1.38	Sandy top soil	High
		l_2	19.7	1.17	2.55	Clayey sand	
		l ₃	335	54.4	56.9	Weathered/fractured	
						basement	
		l_4	44878			Fresh basement	
25	Н	lı	241	1.97	1.97	Sandy top soil	Moderate
		l_2	151	34.8	36.8	Weathered/fractured	
						basement	
		l_3	79606			Fresh basement	

VI. Geo-Electric Sections

Six geo-electric sections were produced showing the subsurface sequence along the established profiles (figures 5a to 5f). Geo-electric layers detected comprised topsoil, clay/clayey sand, lateritic sand, compact laterite, weathered/fractured basement and fresh basement.

The topsoil had resistivity values ranging from $1.9\Omega m$ to $1360.0\Omega m$ and depth ranging from 0.59m to 4.34m. The clay/clayey sand layer had resistivity range of $0.4\Omega m$ to $24\Omega m$ while lateritic sand varied $7\Omega m$ to 16 Ωm . Compact laterite showed resistivity range of $1024\Omega m$ to $3060\Omega m$.

The weathered/fractured basement had resistivity values ranging from $22\Omega m$ to $806\Omega m$ while the detected basement rocks were highly resistive, of the order of $10^3\Omega m$ to $10^5\Omega m$ with unknown depths. Figures 5c and 5f are characterised by structural deformation at respective depths of 8.0m and 4.8m.



Figure 5a: Geo-electric section of the profile along VES 2, 1 & 24.



Figure 5b: Geo-electric section of the profile along VES 14, 13, 10 & 4.



Figure 5c: Geo-electric section of the profile along VES 5, 12, 11 & 19.



Figure 5d: Geo-electric section of the profile along VES 9, 7, 25, 24 & 6.



Figure 5e: Geo-electric section of the profile along VES 8, 20, 21 & 23.



Figure 5f: Geo-electric section of the profile along VES 19, 18, 3 & 15.

VII. Conclusion And Recommendation

The method of investigation adopted by this study has helped in the identification of the aquiferous units and has provided an understanding of the thickness of the aquifer layers and other geo-electric layers, ground water potential and lithologic units within the study area. The second layer mostly constitutes the aquifer units in the investigated area with weathered/fractured basement rocks although a few layers amongst the third and fourth strata were interpreted as conduits for groundwater. The thicknesses of the weathered/fractured basement of VES 2, VES 5, VES 8, VES 14, VES 21, VES 24 and VES 25 (stations) were observed to be approximately 30, 45, 28, 25, 25, 55 and 34 metres respectively which make these seven stations rank topmost for ground water potential within the investigated area. The underground water potential rating of five (5) VES stations were rated low, seven (7) VES stations were rated very low while six (6) VES stations were rated poor. With the classification of the groundwater potential of the study area, the problems of drilling dry holes could be minimized.

From the results of this research, the recommended sites for development of viable boreholes are stations VES 2, VES 5, VES 8, VES 14, VES 21, VES 24 and VES 25. It is therefore suggested that groundwater development through borehole construction in the study area as well as other basement complex terrain should be preceded by geophysical investigation. This will minimize the problems of drilling dry holes and enhance access to groundwater resource in Basement Complex terrains.

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