

Movable Surface Irrigation System Design

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Abstract: Center pivot modification depends on replacing the sprinkler head (sprayer) by polyethylene hoses ending by nozzles.

Field experiments were conducted at the experimental farm of Faculty of Agriculture, in Shams University, to modify sprinkler pivot to work as a moving surface irrigation system. Two different nozzle shapes were selected (trapezoid and triangle) with two different hoses length (25 and 200 cm). Pilot area was divided into two halves, the first was straight furrow, while the second was furrow as well as concentrated with track of pivot wheel, and planted maize.

The main objectives of this study are to modify pivot irrigation system to be more suitable to irrigate trees, and other crops under special conditions, to evaluate the modification system and to reduce the investment costs of the modified system.

Results show that, operating the Movable Surface Irrigation System (MSIS) at low pressure head (1.5 bar), water amount was decreased by (16.8%), the uniformity coefficient for triangle form was 91.6%, pulled hoses (200cm) were better than the short hoses, on the other hand, water use efficiency (WUE) with Movable Surface Irrigation System. system was (2.5 kg/m³) while it was (1.84 kg/m³) with sprinkler pivot system and the Movable Surface Irrigation System. system reduced the hazard of chemigation.

The investment cost of the modified system was reduced as compared with traditional system with little energy required for the Movable Surface Irrigation System. system.

There's no significant difference between the two methods of furrow on grain yield of maize.

I. Introduction

Egypt is mainly an agricultural country in which irrigation technologies plays an important role in supporting national economy. Irrigation water consumes about 85-88 % of the country's water budget for cultivating approximately 8 million feddans with an annual crop area of about 15 million feddans.

Developed irrigation systems are very important for sustainable agriculture, sprinkler irrigation system is one of the most important modern irrigation systems especially in new reclaimed areas, but in special cases this system needs to be modified to be more suitable for this region, **Helweg (1989)** suggested modifications to decrease instantaneous application rates are only suitable for row crops. The traveling trickler system designed for grain crops showed promise of being more efficient, on the other hand, **Wilmes et al. (1993)** reported that, center pivot systems can be one of the most efficient and uniform method of applying irrigation water if the system is properly good designed and managed, also **Broner (2002)** reported that, high-pressure to low-pressure conversion, a change from high-pressure to low-pressure systems, if done properly reduces pumping costs. However, low-pressure systems require sprinkler heads (water-emitting devices) that usually have a smaller radius of throw that results in higher instant application rates. Higher application rates for lower pressures is the main trade-off between high- and low-pressure systems. However, there are several other factors to consider if you change from high to low-pressure systems or to LEPA systems.

II. Material And Methods

Hydraulics:

The basic modification of pivot system depended on replacing the sprinkler heads by P.E. hoses which can be operated at lower pressure.

For that, it's crystal clear that piezometric head reduces along pivot main line because of friction losses. According to dynamic equal, we can see the reserve relationship between velocity of water flow and section area of flow exits.

it's important to mention that wanted discharge is assumed, at this research discharge is assumed (0.5 l/s), while the Piezometric head was measured. And friction losses were calculated according to **Darcy – Weisbach** equation.

A technique characters of simple pivot at Experimental farm, Faculty of Agric., Ain Shams University, for a single tower center pivot irrigation system (48 m) radius, (127 mm) diameter of main line,

thickness of pipe (3) mm, and (75cm) space between holes, according to handbook of pivot technique characters.

$$D = 536.3 [Q^{0.5} / h^{0.25}] \text{ ----- (1)}$$

Where:

D = Inside diameter of outlets (mm)

Q = Discharge of outlets (m³/s)

h = Outlets Pizoemeteric head (m)

From calculations it's clear that change of inside diameter hose is very small (0.02,0.03,0.04,and 0.05 mm). The calculated diameters have very micro changes which are not available at markets which have limited diameters. Therefore, if using the available diameter, it's a must to design the MSIS outfitting. But to achieve this work, the following two steps must be considered:

1 – reducing the diameter to be suitable for calculated diameters.

2 – obtaining small change of calculated diameters.

The experimental calculated begun by selecting five categories of hoses inside diameters (10.5,11,11.5,12,and12.5mm) from calculated diameters to be carried out.

Outfit design of movable surface irrigation system:

Outfit which design contrasts inside hoses which also constructed at lateral pipe of pivot at sprinkler places by using barbed.

Basic components of movable surface irrigation system outfit:

- Polyethylene hose (20mm diameter),
- Hose connection (barbed) (3/4" / 20 mm diameter).
- Cylinder of wood stick (20mm diameter).

Form and cross-section area of hole outlet:

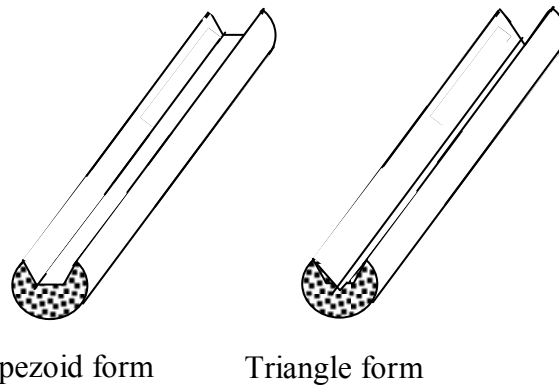


Fig. 1: Two forms in cylinder of wood stick.

Two forms of cross-section area of hole outlets were selected the outlets are excavated along the stream of wood stick cylinder according to designed areas, as shown in Fig.(1)

Trapezoid plus segment of a circle:

From experimental calculation, this form is produced. It depends on excavated linear tunnel at cylinder of wood to give the wanted section of area

$$A_t = ((ab + cd) / 2) L \text{ ----- (2)}$$

$$A_c = 2/3 L \times ab \text{ ----- (3)}$$

Where:

A_t = Area of trapezoid ,mm²,

A_c = Area of segment of circle,mm²,

ab = String of circle of stick wood section (the up base of trapezoid) ,mm,

cd = The down base of trapezoid ,mm,

L = Altitude of trapezoid ,mm, as shown in Fig.(2):

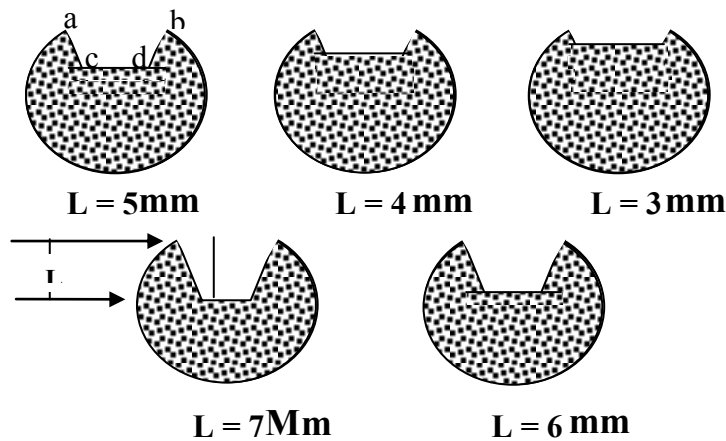


Fig 2 :Cross section of excavated cylinder of wood at trapezoid form.

Triangle plus segment of a circle:

The experiments appear that suitable change for previous gradually diameters were obtained also by changing of central corner. Where, the changeable area can be obtained from relationship between central corner changing and area changing. The rate of central corner changewas 10 degree, beginning with (100, 110,120,130,and 140 degree) as shown in Fig.(3)

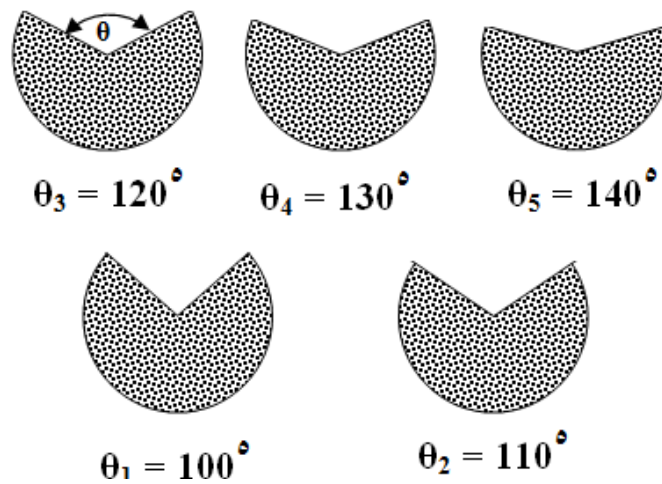


Fig. 3 :Cross-section of excavated cylinder of wood at triangle form

Hose lengths:

For two nozzle shapes, there's two length of hoses were fixed, first length is 25 cm and suspended at 75 cm from soil surface, second length is 200 cm and pulled at soil surface as showed at Fig. (4)

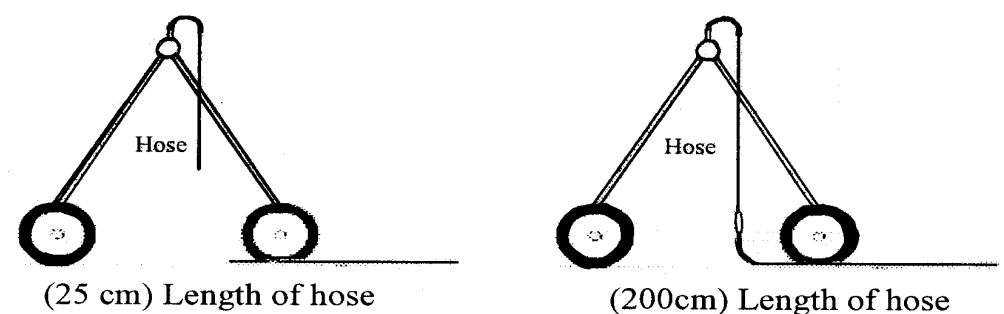


Fig. 4 : Hoses end (measurement points) and Two lengths of hoses .

Calculated graauany area:

$$A_1/\theta_1 = A_2/\theta_2 \text{ -----(4)}$$

$$A_{cn} = (\theta_n/360) \times A_t \text{ ----- (5)}$$

Where: A_{cn} = Area of triangle plus segment circle (mm^2),
 θ_n = Central corner, degree,
 A_t = Total area of hose (mm^2).

Uniformity coefficient evaluation of movable surface irrigation system.ppllication:

Discharge measurements:

Discharge measurements were taken with inflow meter for pump, while for nozzles were taken at next. Samples were taken by selecting 22 from 44 hoses. These samples were taken by received water application at gradual container during period from time according to (Keller and Karmeli, 1975). For reducing experimental error, discharge was measured four times.

Uniformity coefficient was calculated according to (Bralts et al.,1987) .

$$Uf \% = 100[1 - (\Sigma Q_d / Q_x)] \text{ -----(6)}$$

Where: $Uf \%$ = Uniformity coefficient, %,
 Q_d = Absolute deviation of each sample from the mean, l/s, and
 Q_x = The mean of outlets discharge, l/s,

Experiments:

Zea maize was planted under MSIS system at the Experimental Farm of Faculty of Agriculture, Ain Shams University. The last crop is clover. Maize crop (single cross No.10) which is been produced by the Field Crop Dept. ARC, Ministry of Agriculture. The furrow space was 70cm while the plant space along furrow was 25 cm

2-4-1– Soil preparation:

Soil was ridged and planning by two methods [traditional furrow (straight line) and round furrow (with track of pivot wheels)] as showed at Fig.(5).

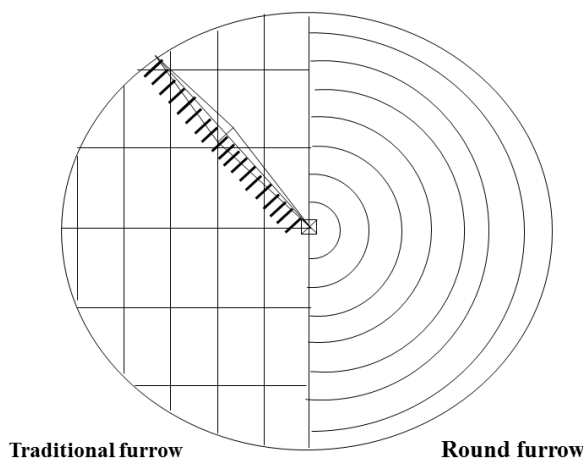


Fig. 5: Traditional furrow and round furrow.

Irrigation requirements:

Irrigation water requirements for maize were calculated using the data of evapotranspiration which were available at the Central Laboratory for Agricultural Climate (C.L.A.C.), Ministry of Agriculture and Land Reclamation. Irrigation requirements were presented in Table (1):

Table (1): Calculated consumptive use (mm/day) of maize using pan evaporation method.

Growth stage	Period	ET ₀ mm/day	K _c	ET _c mm/day	ET _c m ³ /fed./day
Initial	26/6 – 15/7	7.2	0.40	2.88	12.096
Develop.	16/7-16/8	6.69	0.80	5.3	22.26
Mid season	17/8-7/9	6.57	1.10	7.23	30.366
Season end	8/9 -23/9	4.7	0.87	4.09	17.178
At harvest	24/9-15/10	3.97	0.57	2.26	9.492

ET_c = Water consumptive use

Irrigation water was applied weekly and calculated crop consumptive use was calculated (mm/day) according to (Doorenbos and Pruitt, 1977)

$$ET_c = Et_0 \times K_c \text{ ----- (7)}$$

Where:

Et_c = Crop consumptive use, mm/day.

Et₀ = Reference evapotranspiration, mm/day.

K_c = Crop coefficient (dimensionless). for maize was used to calculate the Et_{crop} values, FAO, (1984)

$$\text{-----(8) Irrigation time} = \frac{\text{amount of water applied (m}^3\text{)}}{\text{modified pivot discharge (m}^3\text{/h)}}$$

$$\text{-----(9) } v_i = \frac{(D\pi)\text{Circumference of irrigated area (m)}}{\text{irrigation time (h)}}$$

$$\text{-----(10) } v\% = \frac{v_i}{v_{max}}$$

where:

v_i = Irrigation velocity, m/h.

v_{max} = maximum velocity for center pivot, m/h.

v% = velocity percentage for center pivot, %.

Fertilization program:

Amounts of fertilizers were added by traditional method according to the recommendation of Field Crop Department, ARC, Ministry of Agricultural and Land Reclamation for maize. Field Crop Department recommended 120 unit Ammonium Nitrate 33%N /feddan divided into three doses each of about 130kg/fed of Ammonium Nitrate and 100 kg/feddan of potassium sulphate 48%.

Crop measurements:

The crop samples were taken by selecting three areas (0.5m x 1.4m), the distance of area samples is 16 m starting at the one third center of mainline pivot and finishing at the end. Area samples contained 9 plants, three samples were taken at traditional and round furrow.

Total grain yield (Mg/ha.) and water use efficiency (kg grain/m³) were determined after 110 days from planting when the mean moisture of kernel was 16.4%

- Total grain yield, Mg./ha..
- Water use efficiency, kg grain /m³ water.

Energy analysis:

Energy requirements and energy applied efficiency (EAE) were determined for MSIS according to Batty et. al., (1975) using the following formula :

a) Power consumption use for pumping water (B_p) was calculated as follows:

$$B_p = \frac{Q * TDH * Y_w}{E_i * E_p * 1000} \text{ ----- (11)}$$

Where:

- B_p** = Power consumption ,KW,
- Q** =Total system flow rate,m³/h,
- TDH** = Total dynamic head ,m,
- E_i** = Total system efficiency ,%,
- E_p**= Pump efficiency ,%,
- Y_w**= Water specific weight (taken as 9810 N/m³)

b) Pumping energy requirements (**E_r**) (**kW.h**) was calculated as follows:

$$E_r = B_p * H \text{ ----- (12)}$$

Where:

H = Irrigation time per season (h).

c) Energyappliedefficiency (**EAE**) was calculated as follows:

$$EAE \text{ (kg/kW)} = \frac{\text{Total fresh yield (Kg)}}{\text{Energy requirements (KW.h)}} \text{ -----(13)}$$

Cost analysis:

Cost analysis to evaluate the MSIS, and it was computed according to **Worth and Xin (1983)**.

The total costs are based on 63hectares size according to market price levels of 2004 for equipment and operating irrigation process.

III. Results And Discussion

Modification of pivot system to be more suitable to irrigate different crops is required to redesign some parts, specially the water outlets (nozzles) to improve irrigation efficiency after modification.

Determining the graduated diameters for movable surface irrigation system.:

Changeable diameters can be calculated for many capacities for pivots with different pivot lengths according to the difference in towers number. By using last relationship (1),

Evaluation uniformity of movable surface irrigation system:

Data showed the deviation of hose discharge from the mean discharge along pivot mainline. Also average pressure head of hoses is equal to 5 m and it's nearly constant along pivot. It deviates ranged from 0.25 to 0.5 meter. Beside, the deference between the two lengths of hose does not affected uniformity or pressure head along the pivot. The hoses which have 200 cm length are better compared with others, because the short hose is a basic reason of water erosion beside it's not recommended to apply water for plant because of fungi diseases and chemigation.

Trapezoid form (hoses length 25 cm and 200cm):

Data showed that, water distribution of outlets is nearly constant for four replicates of measurements. Uniformity coefficient is high, it was 92.5% and 87.8% for hoses length 25 cm and 200 cm respectively, which is considered excellent and good according to **(Merriam and Keller, 1978)** and **(IRYDA, 1983)**.

Regarding the mean total discharge for hoses length 25 cm, data showed that the mean total discharge of replicates of MSIS was 46.8 m³/h, and the mean discharge of outlets was constant 0.33 l/s. On other hand, the mean total discharge of hoses length 200 cm was 45 m³/h, and the mean discharge of outlets 0.25 l/s, also the discharge stability beside the pressure head take a vibrated line as shown in Fig. (4). And the deviation of pressure head from the mean ranged between (0.1 , 0.4 meter) and (0.2,0.5 meter) for hoses length 25 and 200cm respectively (Fig.6 and 7).

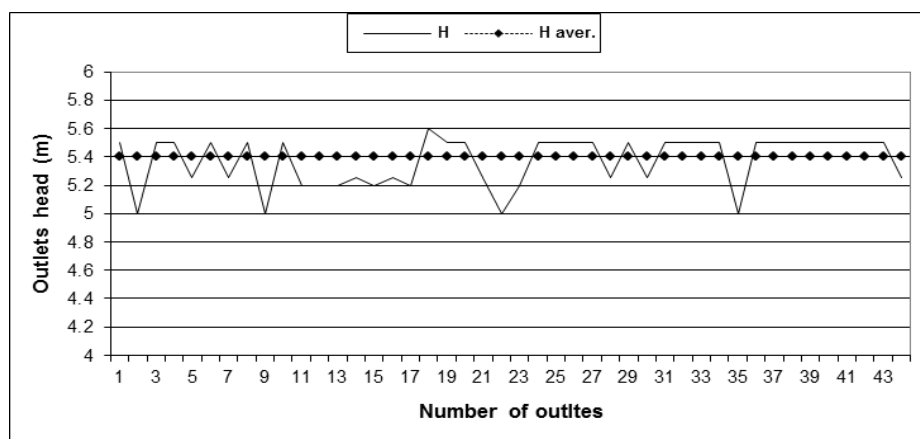


Fig. 6: Deviation of outlets piezometric head about the head piezometric at trapezoid form with short hoses.

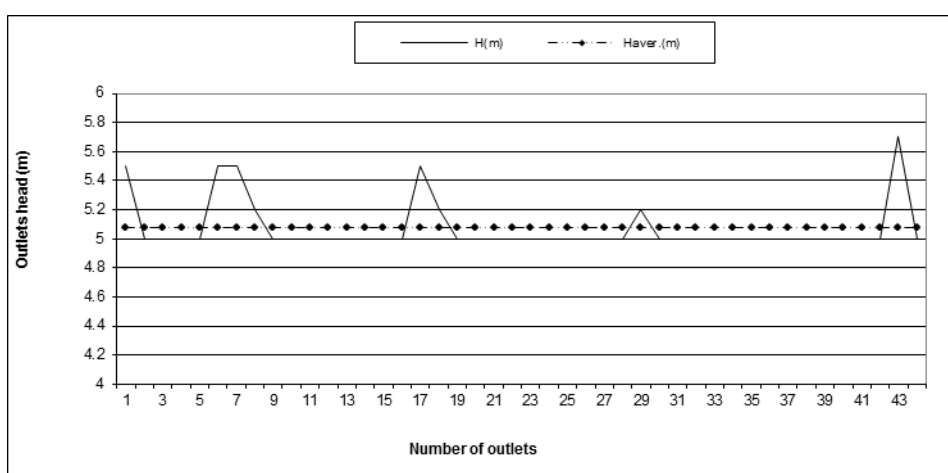


Fig. (7): Deviation of outlets piezometric head about the meanhead piezometric at trapezoid form with long hoses.

Triangle (hoses length of 25 cm and 200 cm) :

Data appeared that, water distribution of outlets is nearly constant for four replicates of measurements. Uniformity coefficient is high, it was 93 % and 90.7 % for hoses length 25 cm and 200 cm respectively, This uniformity is excellent according to (Merriam and Keller,1978) and good according to (IRYDA,1983) for both hoses length.

Regarding the mean total discharge for different replicates for hoses length 25 cm data illustrated showed that, mean total discharge was 55 m³/h. The mean discharge of outlets was 0.33 l/s. While for hoses length of 200 cm, the mean total discharge was 53 m³/hand the mean discharge of outlets was 0.3 l/s. The difference between mean discharge for all of simple tower (total) and mean total discharge was due to experimental errors, which result to difference of discharge measurements. The discharge stability due to the pressure head take a vibrated line as shown in Fig.(6 and 7) and Fig.(6) showed the constant of plotting head pressure. The deviation from the mean ranged between (0.2,0.5 meter) and (0.2 , 0.8 meter) for hoses length 25 and 200 cm respectively. Fig.(8 and 9).

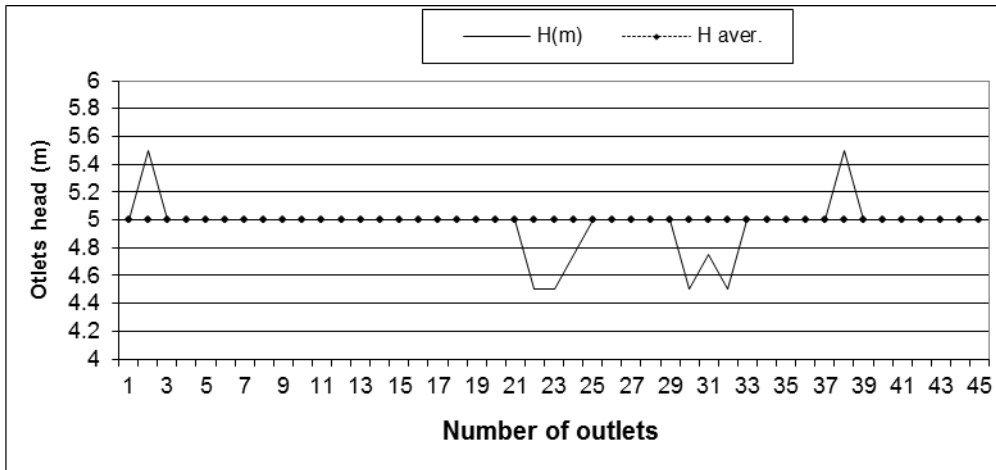


Fig. 8: Deviation of outlets piezometric head about the mean head piezometric at triangle form with short hoses.

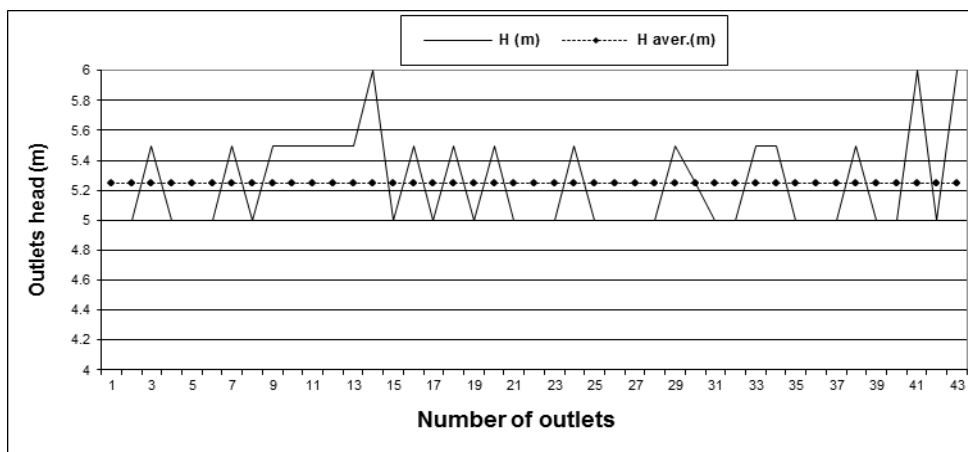


Fig. 9: Deviation of outlets piezometric head about the mean head piezometric at triangle form with long hoses.

Results of growing maize under movable surface irrigation system:

Water distribution:

Water distribution under MSIS was a very important indicator for water application efficiency and system efficiency which was 90 % ,beside amount of applied irrigation water at season (4744 m³ / ha) while it was (5702 m³/ha) under pivot sprinkler systems. (El-Gindy, et al 2003) that means applied water under MSIS lower with 16.8% of applied water under sprinkler pivot. Also, due to the ratios of water stored in the root zone to the water delivered to the field and is thus influenced by the following causes:

- a – Evaporation losses from water flowing on the soil surface or in the air from sprinkler nozzle spray,
- b – Soil surface evaporation during irrigation.

MSIS aspect involved designing a system to be used in conjunction with micro-basin land preparation or furrow diking which prevents runoff and maximizes the use of rainfall and applied irrigation water. Outlets were developed to accomplish both goals. No wind losses result since water is discharged directly into the furrow. Also, protecting plant from water which causes fungal diseases beside from pesticide hazard usage and generally chemigation when injection at MSIS.as showed at Fig.(10).

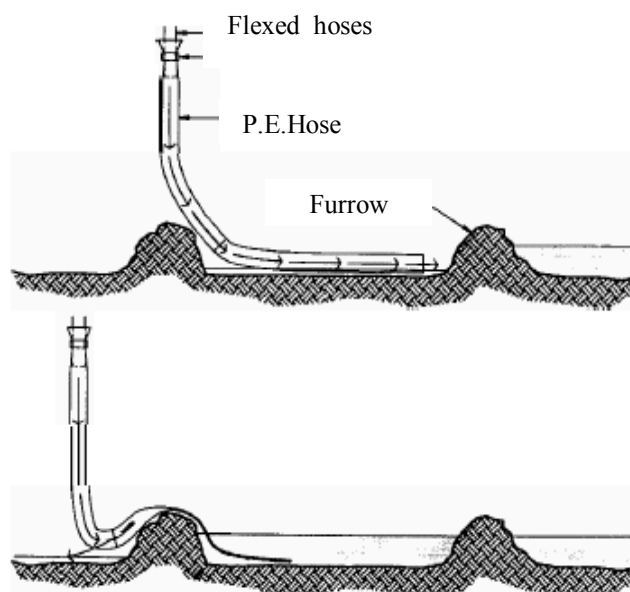


Fig. 10: MSIS outlets designed to be used in conjunction with furrow dikes. The hose prevents wind losses.

Crop yield:

Maize grain yield under modified system was 11.57 Mg /ha for round furrow, while it was 12.37, Mg /ha for traditional furrow. Difference between traditional furrow and round furrow is insignificant. It's important to mention that both maize grain yield of two furrow treatments was good according to (El-Gindy, et al. 2003), while maize grain yield in this study under MSIS was 11.97 Mg/ha. Water use efficiency for maize was 2.5 kg/m³ and 1.84 kg/m³ for MSIS and sprinkler pivot respectively.

Energy analysis:

Table 2: Pump power, energy requirement, and energy applied efficiency for both of sprinkler pivot and MSIS.

Type of energy requirement	Sprinkler pivot	MSIS
Bp (kW)	4	2.95
Er (kW.h)	833	164
EAE (kg / kW.h)	10.34	26.4

Power consumptive use for pumping water (Bp) for sprinkler pivot was (4 kW), while it was (2.96 kW) for MSIS. Beside, pumping energy requirement (Er) was (833 kW.h) for irrigation season under sprinkler pivot when irrigation time during the season was (208.25 h), (El-Gindy et al. 2003). But, MSIS was (164.15 kW.h). Finally, energy applied efficiency (EAE) was (10.34 Kg / kW.h) for sprinkler pivot, while it was (25.5 Kg / kW.h) (27.27 Kg / kW.h) for round furrow and traditional furrow at next, it's clear that energy requirement for MSIS is lower than energy requirement at pivot, it's lower with (26% - 80,3%) for power consumption use for pumping water (Bp) and pumping energy requirements at next. While energy applied efficiency (EAE) of MSIS is higher than sprinkler pivot, it's higher with (60,8%), as shown in Table (2).

Cost analysis:

By calculating both annual fixed and operating costs for MSIS, it becomes crystal clear that MSIS was more economical compared with sprinkler pivot as shown in Table (3). This difference is due to static package sprinklers compared with MSIS fittings, repairs and maintenance costs of hours per season costs beside, to the reduced of energy beside to the decrease labor costs. Data in Table(3) appears that, labor cost for MSIS was lower than sprinkler pivot by (76.6%), cost of one m³ of water in LE for MSIS was lower than sprinkler by (20%), and finally, cost of unit production unit (LE/kg) for MSIS was lower than sprinkler pivot by (36%).

Table 3: Cost analysis for both of MSIS and sprinklerpivot irrigation systems.

Item	pivot	MSIS
Pivot towers cost ,LE/ha	4285.7	4285.7
Nozzles cost ,LE/ha	36	6.3
1 – Capital cost ,LE/ha	4321.7	4292
2 – Annual fixed cost, LE/year		
Deprecation	144	143
Interest	403	400
Taxes and Insurance	64.8	64.4
Subtotal	611.8	607.4
3 –Annual operating costs, LE/ha		
Labor	300	70
Energy	120	22.5
Repairs and maintenance	120.65	42.9
Subtotal	549.65	135.5
Annual Total Costs, LE/ha	1161.5	742.8
Cost of one m³ of water (LE / m³)	0.20	0.156
Cost of production unite (LE / kg)	0.1	0.064

IV. Conclusions

- 1- Felexbility of derived relationship to calculate the suitable diameters of outlets for many pivot towers.This relationship is:

$$D = 536.3Q[0^{-5}/ h^{0.25}]$$

- 2- MSIS obtained both of pivot advantages and modified surface irrigation.
- 3- Traingle form was the more suitable thantrapzioed form, due to facility and flexibility design. Also, micro of changbale diameters which were obtained at trangle.
- 4- Category of diametres were distributed at one half of pivot mainline then the next half, because of elevation difference.
- 5- Uniformity coffiecent of two forms and two lengths was high .
- 6- Total dynamic head was reduced from (3 – 4 bar) at sprinkler pivot to (1.5 – 2 bar) at MSIS. And consequently, at next saving energy requirment and irrigation costs.
- 7- The a mount of irrigation water applied by using MSIS was 16.8 % less compared with sprinkler pivot systems.
- 8- Pulled hoses were more suitable than short hoses.
- 9- Chemigation was more safe with MSIS which reduce hazarad of wind evaporation, besides, preventing of green plant pollution with pesticides.
- 10- Water use efficiency was increasedas a result to saved wind lossesof water.
- 11- There's no optical difference between traditional furrow and concerting furrow because of plants density and flexibility of PE hoses.
- 12- Flexibility of MSIS to irrigate shrubs, small trees, and plants which are sensitive to water with any fungal disease or flowers falling.

Reference

- [1]. Batty, J. C.; S. N. Hamad and J. Keller (1975).Energy inputs to irrigation. J. of Irrig. Drain. Div., ASCE, 101(IR4):293-307,USA.
- [2]. Barlts,S.V.;D.M,Edwards,andP.-Wu(1987).Drip Irrigation design and evaluation based on staticuniformityconcept. In Aduncein Irrigation (ed).D.Hillel,New York Academic Press Inc.,pp67-117.
- [3]. BronerI.(2002),Center pivot irrigation system ,No.4.704.,
- [4]. www.ext.colostate.edu/.
- [5]. Doorenobs ,J.and W.O. Pruitt (1977).Guidelines for predicting crop water requirements .FAO Irrg.and Drain. paper24.Rome ,Italy: p 156.
- [6]. El-Gindy, A. M.; M. F. Abd El-Salam; A. A. Abd El-Azize and E. A. El-Sahar(2003),Some engineering properties of maize plants, ears and kernels under different irrigation system.,J. Agric., Sci., Mansura Univ., 28(6):4339-4360.
- [7]. FAO (1984).Guidelines for predicting crop Water requirements. FAO Irrigation and Drainage ,paper No,24.
- [8]. Helweg,O.J(1989).Evaluating the travelling trickler center pivot., ICID-Bulletin.38:1, 13-20.
- [9]. IRYDA (Instituto de ReformaYdesarrolloAgrario),1983,Normas paralaredacción de proyectos -deriegoLocalizado.Ministerio de Agricultura,Pesca Y Aimenta-ción, Madrid,Spain.
- [10]. Keller ,J.andD.Karmeli(1975).Trickle irrigation design rain bird sprinkler manufacturing crop.,GlendorCalfi, 91740 USA: 24-26.(cited from Rawlines,(1977).sda.gov/personnel/pdfs/Center%20Pivot%20Irrigation.pdf
- [11]. Merriam,J.L.andJ.Keller(1978).Farm irrigation systems evaluation :Aguid for management UTAH Sates University .Logan, Utah,USA
- [12]. Wilems,G.J.;D.L.Marten;R.J.Supalla,(1993),Decision support system for design of center pivots, ASAE Transaction, 37(1): 165-175
- [13]. Worth,B, and J.Xin(1983).Farm mechanization for profit, Granada Publishing.UK.p269.