

External Flow Analysis over One-box form (Algerian Commercial Vehicle) Using CFD

Abdessamed Kacem, Ali Najim Abdullah

¹Ministry Of Higher Education/ Baghdad University

²Ministry Of Higher Education/ Al-Rafidain University College

Corresponding Author: Abdessamed Kacem

Abstract: Computational fluid dynamic software ANSYS Fluent 15.0 is used to predict the physical parameters on the external surface of a vehicle. The simulation of the wind tunnel experiments using the above CFD package would be carried out. To study the aerodynamic influence of vehicle segments are considered as one-box form Bus model (S.N.V.I 100V8). As this model provided with the extremities in the design of vehicle category in summarizes these results in a broader sense to understand the aerodynamics of such profile. A wind tunnel experiments consists of physically testing the model in a simulated environment. It is a closed environment in which air is blown across the model at a constant velocity. As the air passes over the vehicle, it follows the streamlines pattern present on the body. This causes a change in pressure and velocity characteristics across the model. By studying the pressure and velocity variations across the model, the drag and lift coefficient could be predicted.

Key words: CFD, Ansys, Fluent, External flow field, One-box form bus model, Drag coefficient, Lift coefficient.

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I. Introduction

An accurate vehicle model an accounts are related to the accuracy in the velocity and pressure variations across the body during testing. To obtain correct results, a true representation of a vehicle is tested in a simulated wind tunnel experiment ^[1]. In real world, full size vehicle models are tested in a wind tunnel to obtain its behavior as shown in figure (1).

II. Grids and Boundary Conditions

Vehicle model is created using ANSYS Fluent 15.0. This model is an approximation to the realistic vehicle and considered for the numerical (CFD) analysis, two-box form to a study the external flow characteristic and the effect of vehicle body profile on it. The computational domain is discretized into 256327 tetrahedral elements for one-box form, as shown in figure (2).

As shown in figure (3), the vehicle is placed approximately in the middle of the numerical model of the wind tunnel in the length as well as in width. There is a ground clearance in between the floor the vehicle and the bottom wall of the wind tunnel. The tunnel wall and the vehicle body are considered as typical wall boundary conditions. At the inlet of the wind tunnel, a constant mean velocity of 45 m/s or 160 km/h is applied and the outlet of the wind tunnel is considered as an outflow boundary. For solving the flow and turbulence parameters, a three dimensional finite volume numerical method and a standard k-ε turbulence model based on commercial code ANSYS Fluent 15.0, are used for analysis.

III. Numerical formulation

For solving the standard variables u, v, w, k, ε and T, three-dimensional Navier-Stokes equations for steady, turbulent, and incompressible flow ^[2] can be written as:

1-3-1 Governing Equations

Mass (continuity) equation:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0 \quad (1)$$

Momentum equation:

$$\frac{\partial}{\partial t} (\rho u_i) + \frac{\partial}{\partial x_j} (\rho u_i u_j) + \frac{\partial P}{\partial x_i} - \frac{\partial \tau_{ij}}{\partial x_j} = 0 \quad (2)$$

Energy equation:

$$\rho \frac{\partial}{\partial t} (\rho H) + \frac{\partial}{\partial x_j} (\rho u_i H - u_i \tau_{ij}) = 0 \quad (3)$$

Where the stress tensor τ_{ij} ,

$$\tau_{ij} = \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] - \frac{2}{3} \mu \frac{\partial u_j}{\partial x_i} \delta_{ij} \quad (4)$$

1-3-2 Turbulence modeling

The standard k-ε turbulence model [3] is used which contain two equations one for turbulence kinetic energy and the other for its dissipation rate obtained from the following equations respectively:

$$\rho \frac{\partial k}{\partial t} = \frac{\partial}{\partial x_i} \left[\left(\mu + \frac{\mu_t}{Pr_k} \right) \frac{\partial k}{\partial x_i} \right] + \left(2 \mu_t \delta_{ij} - \frac{2}{3} \rho k \delta_{ij} \right) \frac{\partial u_j}{\partial x_i} - \rho \varepsilon \quad (5)$$

And....

$$\rho \frac{\partial \varepsilon}{\partial t} = \frac{\partial}{\partial x_i} \left[\left(\mu + \frac{\mu_t}{Pr_k} \right) \frac{\partial \varepsilon}{\partial x_i} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} \left(2 \mu_t \delta_{ij} - \frac{2}{3} \rho k \delta_{ij} \right) \frac{\partial u_j}{\partial x_i} - C_{2\varepsilon} \rho \frac{\varepsilon^2}{k} \quad (6)$$

In the above equation, the last three terms on the right hand side shows the diffusion generation, and the dissipation rates of ε and the turbulent viscosity derived is,

$$\mu_t = C_\mu \rho \frac{k^2}{\varepsilon} \quad (7)$$

Where $C_\mu=0.09$

The simulation results are obtained under the convergence criteria of 1.1^{-10} for the residuals of u, v, w, k and ε. The drag coefficient can be calculated using the following equation.

$$C_D = \frac{F_D}{\frac{1}{2} \rho_\infty V_a^2 A_f} \quad (8)$$

Where F_D is the force acting in the direction of air flow on the frontal area of the vehicle body and $(\frac{1}{2} \rho_\infty V_a^2)$ is free stream dynamic pressure. In the present solution, a semi-implicit method for pressure linked equation (SIMPLE) is used. Figure (4) shows the flow chart for external flow modeling that illustrates the options used in ANSYS Fluent 15.0 software [4].

IV. Results and discussion

The velocity increasing is smoother when compared to that of two and one-box form car models. This is attributed due to the smooth profile changes across the hood and the roof. There is a subtle change in the velocity at the rear end as the flow separation occurs, as shown in (Figure 5). The pressure contour plot along z-axis at a distance of 1m from the side face (figure 6) indicates details about the low-pressure zones. Air drag coefficient for (S.N.V.I 100V8) Bus model is shown in (figure 7) and the Lift coefficient for (S.N.V.I 100V8) Bus model is shown in (figure 8), such values are amended in the same study.

V. Conclusion

In the case of one-box form model, low-pressure pockets are present at the top and bottom of the vehicle. This differential pressure is almost negligible that keeps the vehicle on ground.

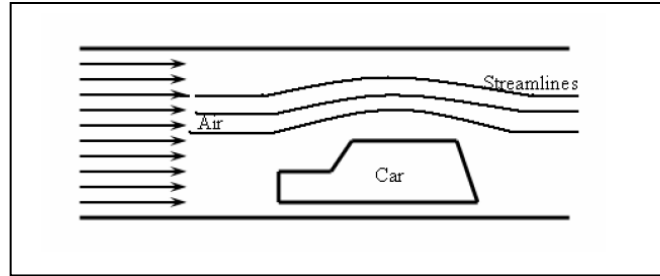
Notations

- A: The model frontal area (m²).
- C_D: Drag coefficient.
- F_D: Total drag force(N).
- V_∞: Undisturbed air flow (m/s).
- g : Gravitational acceleration (m/s²).
- ε : Dissipation rate.
- ρ : Density(Kg/m³).
- σ : Normal stress.

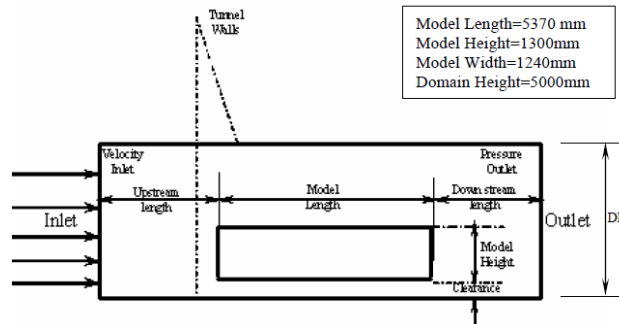
ν : Kinematic viscosity.
 μ_t : Additional viscosity due to turbulence.
 τ_{ij} : Stress tensor.

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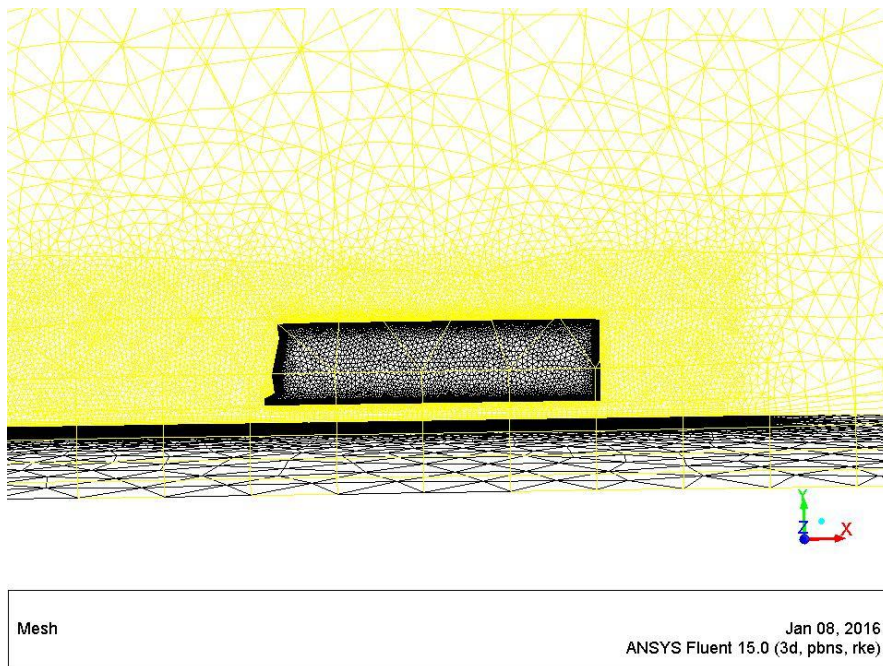
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Figure(1): Wind tunnel testing



Figure(2): Grid display for One box form car model



Figure(3): ANSYS Fluent 15.0 for (S.N.V.I 100V8) Bus model

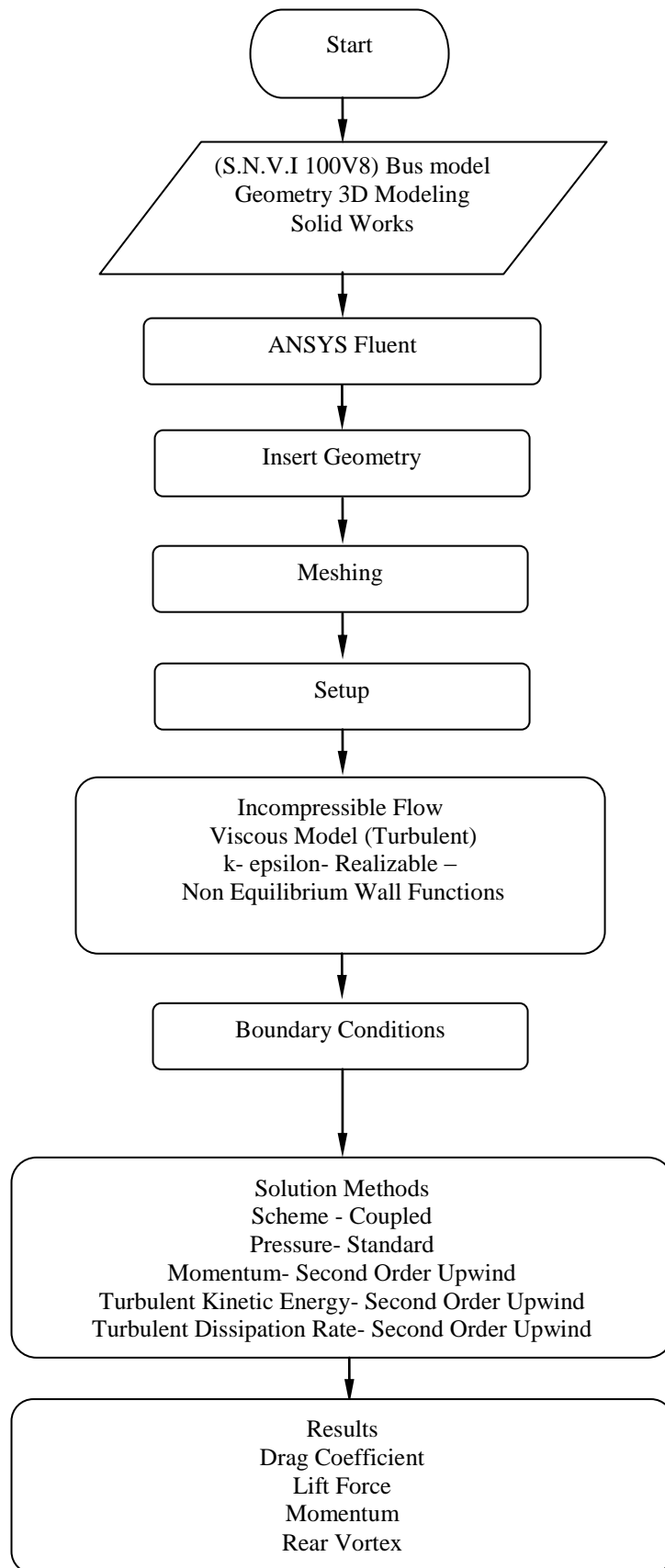


Figure (4): Shows the flow chart for the external flow modeling That illustrates the options used in ANSYS Fluent 15.0

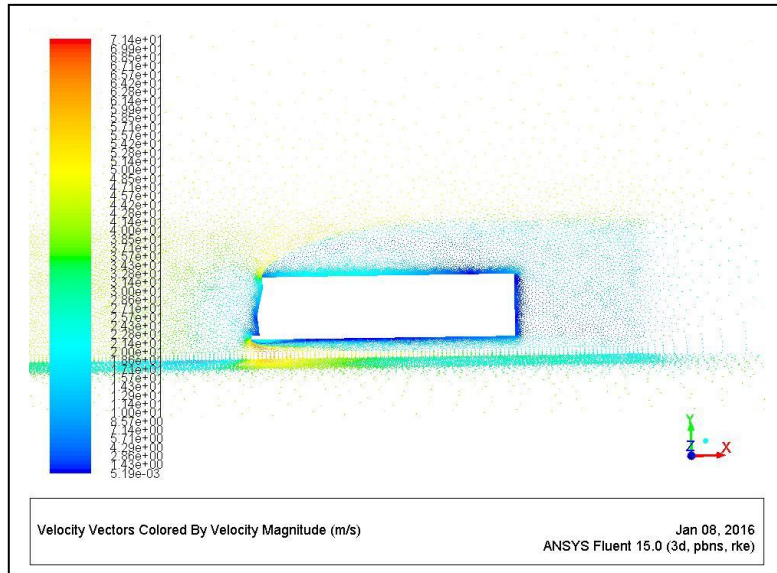
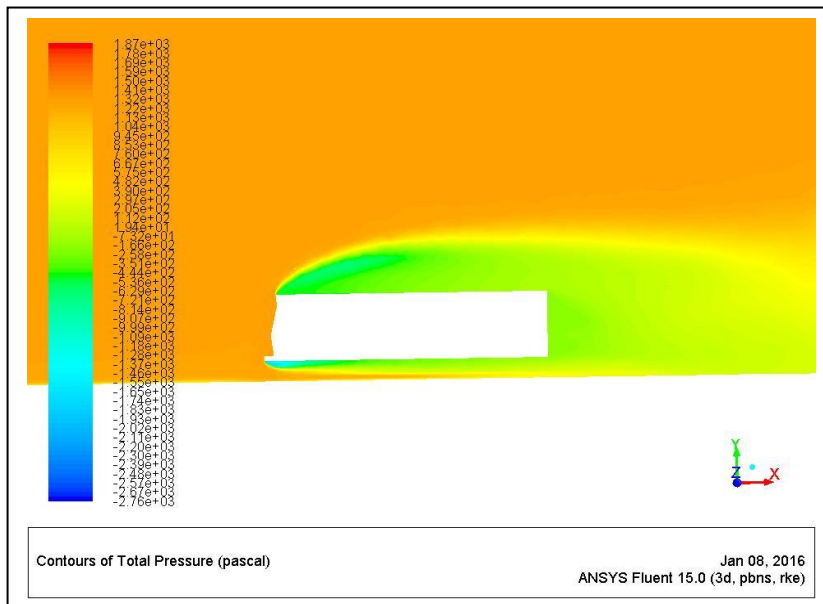


Figure (5): Velocity vectors on the surface of vehicle (m/s)



Figure(6): Pressure contour for vehicle at a plane along z-axis=1 m (pascal)

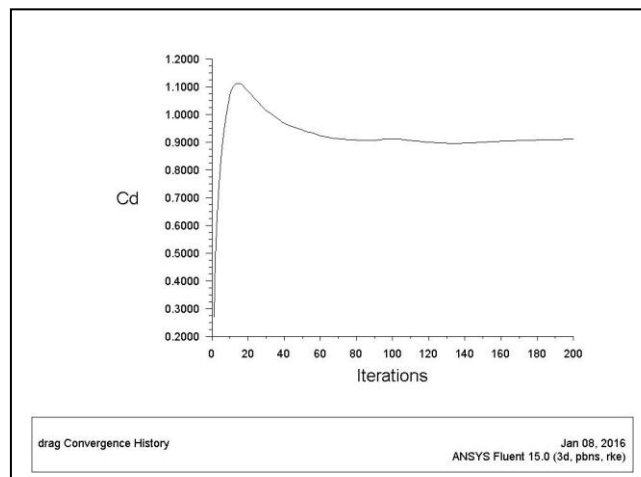


Figure (7): Air drag coefficient for (S.N.V.I 100V8) Bus model

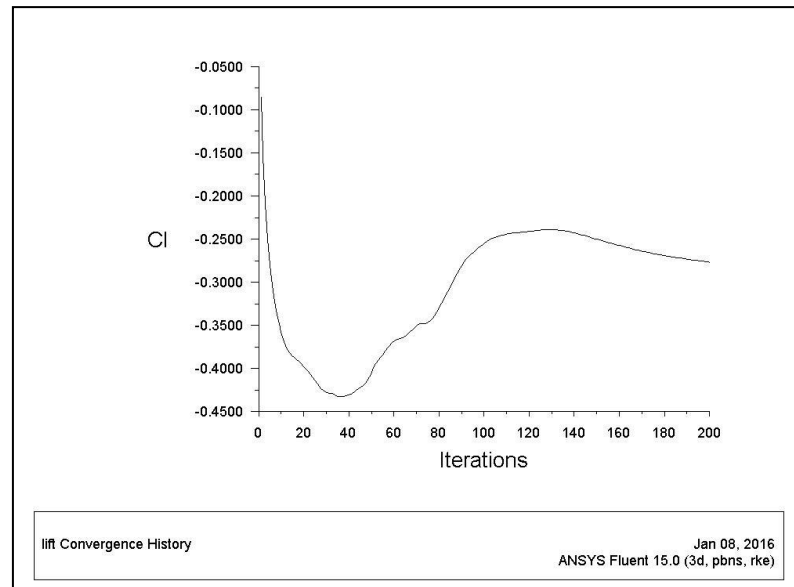


Figure (8): Lift coefficient for (S.N.V.I 100V8) Bus model

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