

## Analysis of The Effect of Polypropylene Polymer (Crushed Plastic Waste) On Oven Dried Laterite Bricks.

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**Abstract:** The sandcrete blocks have been a major material for the construction of structures in Nigeria. This material has provided a means of constructing walls and partition. However, the sandcrete blocks also have the disadvantage of cost and unavailability of materials such as granite, cement and other combining aggregates. Laterite, a readily available material can be efficiently used to produce Laterite bricks which can be fired to improve its structural properties. The incorporation of wastes such as polymer into the production of bricks can contribute to a more stable constructional material. The main advantage which is the reduction of nonbiodegradable materials dominating dumpsites and landfills. The main idea of this research is to focus on the possibility of creating laterite bricks with properties improved through the addition of waste plastic. Study was carried out on the effect of the plastic wastes on the compressive strength, flexural strength, loss of weight and shrinkage due to heating. The results showed that properties such as compressive and flexural strength decreased upon increasing the polymer content but remained within the acceptable limits. Based on the results of this study, the use of waste plastic in bricks is recommended but to a limit of 5%.

**Keywords:** laterite bricks, polypropylene polymer bricks, crushed plastic laterite bricks.

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Date of Submission: 22-11-2020

Date of Acceptance: 07-12-2020

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### I. Introduction

Before the discovery of limestone and the advent of cement, mankind has relied on simple earth made bricks for the construction of various structures and artifacts some of which still stands today. These bricks were mostly made of well graded Laterite soils without additives which were mixed with a proportion of water to obtain a paste and were cast or moulded into different shapes. Although these bricks had the advantage of being solid and had a very good resistance to shear forces, they still were brittle and deteriorated in the presence of water. These made them very unsuitable for construction in marshy areas, lands prone to intense flooding and for certain other constructions such as dams and bridges.

In modern times, it is now known that these bricks can be baked in temperature regulated kilns to improve some of their properties some of which include their tensile strength and water resistance. Compressed soil masonry blocks formed using moist soil compacted mechanically have now gained popularity. Benefits of earth blocks in this manner include improved strength and durability as compared to adobe while maintaining significantly low embodied energy levels than alternative materials. However, problems arise still from the material's low tensile strength, brittle behaviour and deterioration in the presence of water. Stabilization by a hydraulic binder such as cement, lime or combination of the two can significantly improve water resistance and strength to some extent [36].

Solid waste management especially the huge quantity of waste plastics is one of the major environmental concerns nowadays. Their employability in brick making in form of fibres (plastic fibre-Laterite bricks) as one of the methods of waste management can be investigated through a fundamental research.

Also, previously carried out researches have shown that most studies on natural fibres are focused on cellulose based fibres obtained from renewable plant resources except in the case of animal fibre and in another case of plastic fibre and polystyrene fabric. In this context, for the plastic fibre-Laterite bricks to be more widely applicable, a systematic quantification of the relevant physical and mechanical properties is crucial; to enable an objective evaluation of the material's response to actual field conditions. This research project aims at highlighting the salient observations from the investigation of a systematic study on the effect of embedded plastic fibre on the performance of stabilized bricks [23].

## II. Materials and Methods

### Polypropylene

Polypropylene is a polymer that belongs to the group of polyolefins which are partially crystalline and non-polar having properties similar to polyethylene but is slightly harder and more resistant to heat. It is the second most widely produced commodity plastic used in a variety of applications including packaging and labelling, textiles (e.g. ropes, thermal wear, and carpets), stationery, plastic parts and reusable containers of various types, laboratory equipment, loudspeakers, automotive components, and polymer banknotes. An addition polymer made from the monomer propylene, it is rugged and usually resistant to any chemical solvent, bases and acid [17].

The plastic wastes are to be derived from disposed or damaged plastic chairs. These materials were obtained from Shagamu Ogun state. They were collected and transported to the crushing factory at Ijebu Ode where they were first fed into the crusher which pulverized them into granules. They were further passed into water which removed contaminants and deleterious materials.

### Soil

The laterite soil used for this research was obtained at a laterite deposit in Institute of Food Security, Environmental Resources and Agricultural Research (IFSARER), Federal University of Agriculture, Abeokuta (FUNAAB), Ogun State, Nigeria.



**Figure 1:** Sample of crushed plastic polymer.



**Figure 2:** Sample of laterite obtained

### Water

The well water was obtained near the casting site which was used in mixing and preparation of brick cubes. The water was clear, free from physically settleable and suspended particles, potable and satisfied the requirements for water according to the standards stated in Methods of test for water for making concrete, BS 3148, British Standard Institution, 1980.

### Mix Details and Proportions

The brick used for this study consists of composites of Laterite and water. The design mix ratio was 1:25 and the water-laterite ratio was 0.5. The brick samples used for evaluating compressive strength ( $T_A$ ) had a dimension 10 x 22 x 11 cm while those for flexural tests ( $T_B$ ) had dimensions 22 x 22 x 11 cm.

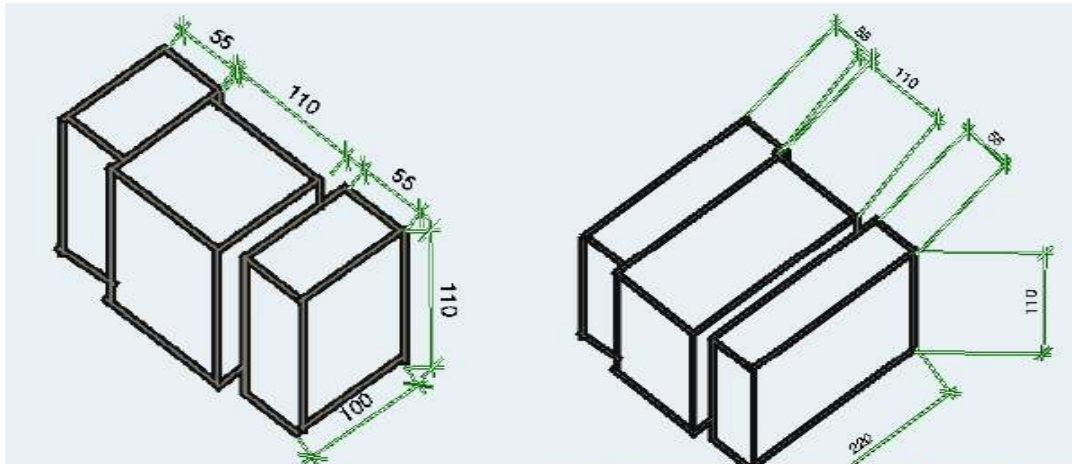


Diagram 1: Dimension of Clay Brick (T<sub>A</sub>)

Diagram 2: Dimension of Clay Brick (T<sub>B</sub>)

**Procedure for Casting of Bricks**

Batching the constituents by weight: Batching by weight eliminates error due to variations contained in a specific volume. Regular inspection and calibration of the equipment must be done in order to provide a consistent batch of aggregate between mixes. The production of bricks began with the control samples followed by the mixture contents, varying the percentage replacement of laterite aggregates by the polypropylene plastic fiber. The percentage replacements considered are 0%, 5%, 10% and 15% of the laterite aggregate with crushed plastic.

Percentage replacement (%)	Total number of bricks	Number of bricks (T <sub>A</sub> )	Number of bricks (T <sub>B</sub> )	Mass of soil (T <sub>A</sub> )	Mass of soil (T <sub>B</sub> )	Total mass of soil	Total mass of polymer
0	9	6	3	30.0	30.0	60	0
5	9	6	3	28.5	28.5	57	3
10	9	6	3	27.0	27.0	54	6
15	9	6	3	25.5	25.5	51	9

Table 1: Mix details

**Mechanized Forming Process**

The Hydraform brick making machine MODEL M8DE MFD 2014 was used for making brick samples used for this research. After the laterite has been mixed with plastic at the required percentage and water added to the aggregate, the upper arm of the machine is raised with the aid of a hydraulic gear revealing the form chamber, the mixture is batched by weight and carefully poured into the chamber. Compression is carried out by both of the lower and upper arm with a pressure of 2200Psi (150bar) after which the upper arm is again lifted and the lower arm raised to lift the moulded brick out of the chamber. Brick mixture with three levels of polystyrene granules were investigated to determine their compressive and flexural strength.

**Drying**

The wet brick from the moulding machine contain 5%-15% moisture. Before the commencement of oven drying, the samples were first dried in the open air for 14 days to reduce its water content.

**Oven Drying**

The drying of Laterite bricks in oven is adopted to further reduce the water content of Laterite bricks or other ceramic products. Drying in an oven or kiln controls many important properties of the finished ware. Some of these properties include Mechanical strength, Abrasion resistance, dimensional stability, resistance to water, fire and chemical.

**Drying Process**

The brick was dried in an oven for 48 hours. The oven was charged by electricity to a temperature of 105°C. The oven drying of plastic bricks intends to improve durability through sintering which can be seen as the bonding mechanism of laterite particles. The key to oven drying is to strictly ensure that the temperature of

the oven is maintained at the required temperature for the period of time through which fusion is improved and partial vitrification occurs but viscous fusion is avoided. Similar to kilns, the oven had a temperature sensor equipped to monitor and control the heating temperature. Near the end of the heating process, the oven was turned off to accomplish the flashing process. Flashing means the drying temperature was reduced [17]. After the heating in the oven for the required time period, the bricks were cooled for 24 hours in open air before any test was carried out on them. Cooling is an important stage in brick manufacturing as it has a significant effect on the colour of the Laterite material.

### Tests Performed on Laterite Bricks

**Compressive Strength Test:** this is an utmost important test which gives an idea about all the characteristics strength of the brick. The compression test was carried out on the specimens at the end of 7 days and 28 days of curing.

Compressive strength =  $P/A$

Where, P = Failure load (N)

A = Cross sectional area ( $\text{mm}^2$ )

Three trial tests were carried out average of which was used for determining the strength of the bricks.

**Flexural Strength Test:** It is loaded unlike compression or tensile test; flexural test does not measure fundamental properties of materials. When a test specimen is placed under flexural loading, all the fundamental stresses are present.

Modulus of Rupture =  $\frac{3Pa}{bd^2}$  ..... 1

Where

b = measured width of in cm of the beam,

d = measured depth in cm of the beam at the point of failure,

L = Length in cm of the supported beam

P = maximum load in KN applied to the beam.

**Water Absorption Test:** The purpose of this test method is to provide a means for comparing relative water absorption tendencies between bricks of different mix proportions. The brick after casting was air dried for 14 days and further oven dried for 2 days. This weight was then noted as the dry weight ( $W_1$ ) of the block. After which the specimen is to be submerged in water for 24 hours. Then the weight would then be noted and water absorption would be thus calculated.

water absorption (%) =  $\frac{W_2 - W_1}{W_1} \times 100$  ..... 2

Where,

$W_1$  = Oven dried weight of brick in grams.

$W_2$  = weight of block after immersion in water for 24 hours. [5].

**Linear Shrinkage:** was obtained by measuring the length of the sample before and after oven drying using a caliper with a precision of  $\pm 0.01$  mm, according to the standard ASTM C326 [4]. The firing linear shrinkage (before and after firing) expressed as a percentage and calculated according to the following formula presented as the results were more readily available.

Firing shrinkage (%) =  $\frac{L_{\text{dried}} - L_{\text{fired}}}{L_{\text{dried}}}$  ..... 3

Where,

$L_{\text{dried}}$  is the length of the oven dried sample (mm)

$L_{\text{fired}}$  is the length of the fired sample (mm).

Firing shrinkage was determined by measuring the physical dimensions of the specimens before and after firing.

### III. Results and Discussion

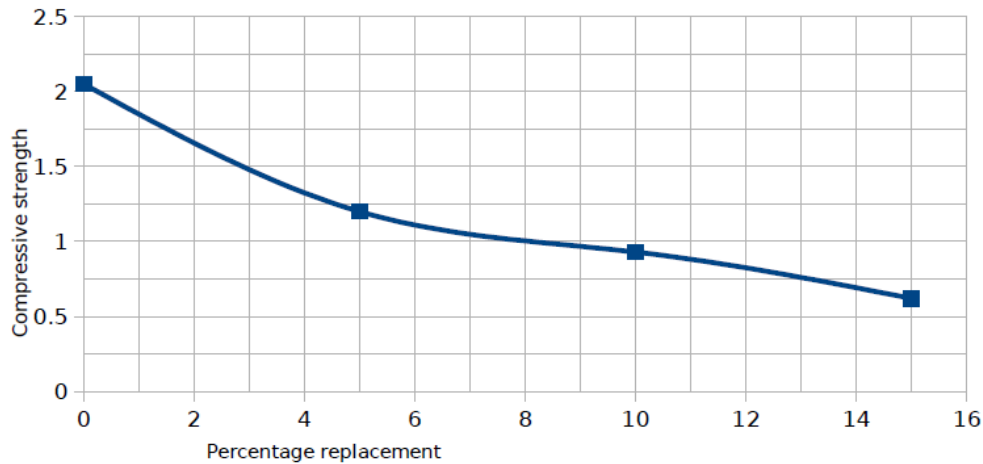
**Compressive strength:** this greatly depends on the amount of plastic waste in the fired brick specimens and the firing temperature. In addition, compressive strength of specimens decreased upon increasing the proportions of plastic

polymers. The decrease was caused by the following;

- Differences in grain size of laterite and polymer granules.
- Weak bond between the laterite grains and polymer granules.

The test results showed that the highest compressive strength was  $2.05 \text{ N/mm}^2$  for 0% waste plastic additive. The result indicated that the compressive strength of oven dried Laterite bricks is inversely proportional to the

containing amount of plastic polymer. The value decreases progressively up to a minimum of 0.6N/mm<sup>2</sup> for 15% plastic polymer replacement.



**Diagram 3:** Graph showing the compressive strength of laterite brick samples

**Shrinkage:** this is related to loss of water among Laterite particles resulting in the closer packing of granules and resulting shrinkage. During heating, ceramic particles fuse together leading to greater proximity and thus enhancing linear shrinkage. It is considered that the reduction in firing shrinkage of brick material had a positive impact on its load bearing. Large shrinkage could result in cracks and dimensional effects. Results showed that the firing shrinkage increased with an increase in proportion of plastic polymer with the highest proportion (15%) developing visible cracks. Shrinkage is normally an important factor to determine the degree of densification during firing. Bricks must have a firing linear shrinkage lower than 8% in order to retain good mechanical performance [37]. The results showed that the lowest linear shrinkage occurred in the control Laterite bricks having no

addition of plastic polymer while the highest value of 4.25% occurred in 15% polymer replacement. The linear shrinkage for all brick samples is within the safe limits for industrial production as indicated in ASTM C326 however the cracks developing in higher percentage replacements. It can be seen in figure 4.2 below that for all the

additives tested, linear shrinkages are below 8%. In addition, the lower these results, the better the final product's properties.

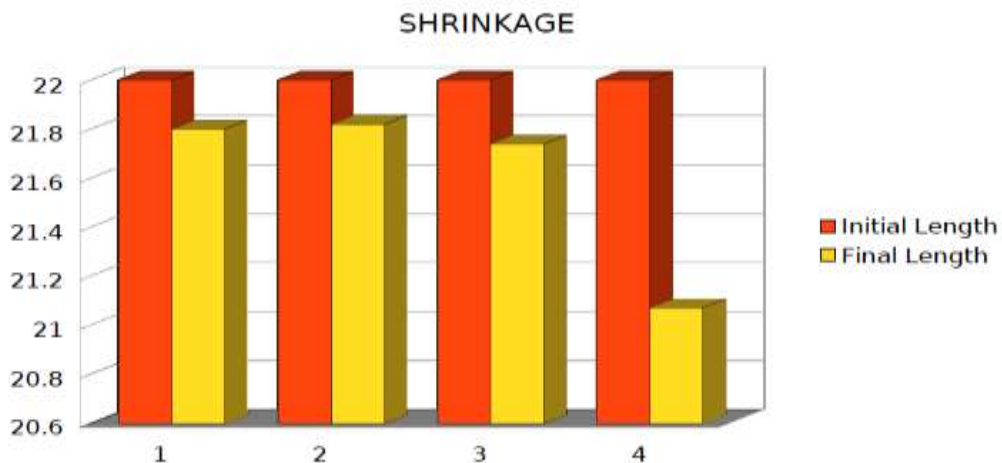
$$\text{Firing shrinkage (\%)} = \frac{L_{\text{dried}} - L_{\text{fired}}}{L_{\text{dried}}} \times 100 \quad \dots \dots \dots 3$$

$L_{\text{dried}}$

Where

$L_{\text{dried}}$  = Length of brick sample before oven drying,

$L_{\text{fired}}$  = Length of brick sample after oven drying.



**Diagram 4:** Chart Showing the Average Shrinkage of bricks having varying proportions of polypropylene.



**Weight loss:** the oven dried Laterite bricks was dependent on the quantity of polymer contained. The greatest weight loss was observed to be that of 0% polymer replacement. This was caused by dehydroxylation and also organic or carbonaceous matter burnt off during the heating process. From Figure 4.3, it was observed that the weight loss of oven dried Laterite bricks decreased upon increasing the quantity of polymer additives.

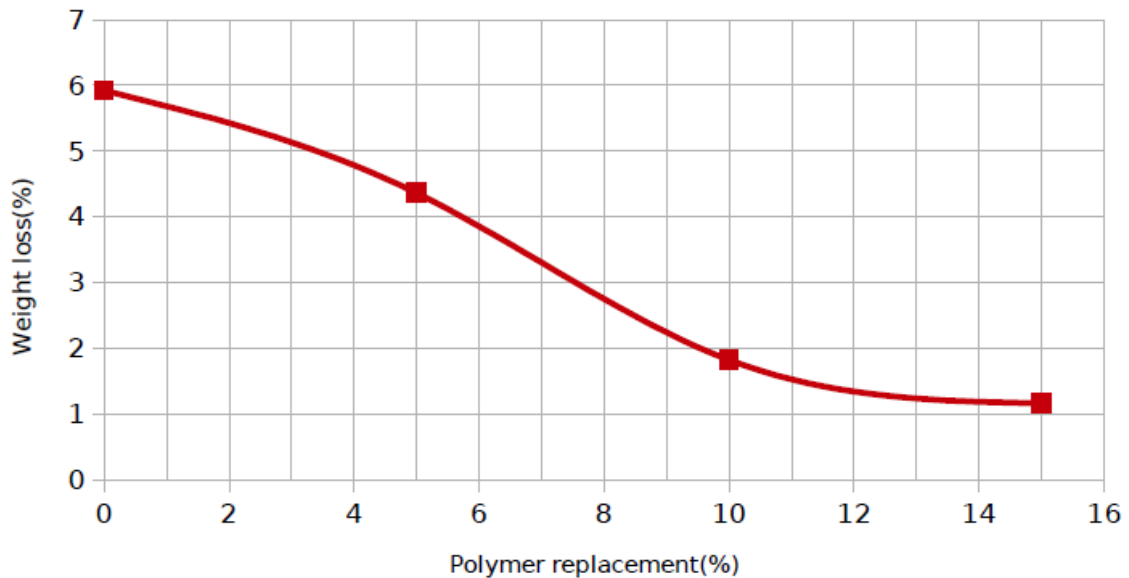
$$\text{weight loss (\%)} = \frac{W_1 - W_2}{W_1}$$

Where

$W_1$

$W_1$  = open air-dried weight of bricks in grams.

$W_2$  = Oven dried weight of bricks in grams



**Diagram 5:** Graph Showing Weight Loss of various Laterite bricks

**Flexural Strength:** noticeable decrease was observed in flexural strength as the polymer content was increased. Modulus of rupture of the oven dried bricks similarly increased with an increase in polymer content. The explanation for this is, due to the reactions that occurred within the samples during the heating process. The brick samples having a higher quantity of plastic polymer had visible cracks after heating for 48 hours which greatly served as a weak point within the body of the brick samples. The test results showed that the highest flexural strength was 4.23N/mm<sup>2</sup> for 0% polymer additives and the lowest, 2.02N/mm<sup>2</sup> for 15% polymer additives. The results showed that the flexural strength of oven dried Laterite bricks is dependent greatly on the amount of waste plastic addition. The values of which decreased progressively from 4.23N/mm<sup>2</sup> to 2.02N/mm<sup>2</sup>,



**Figure 3:** Flexural Strength Test Set Up

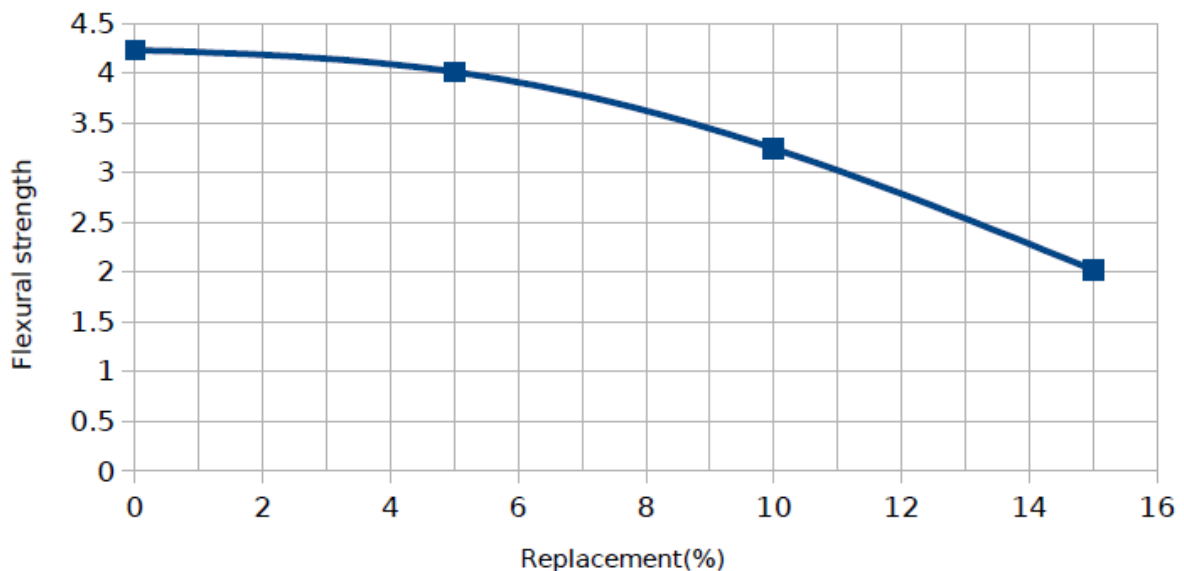


Diagram6: Graph showing flexural strength of brick samples

#### Collapse of oven dried bricks

Mainly due to the absence of a binder in the mixture used in moulding, the Laterite bricks collapsed into pieces after a few hours of immersion in water. Although, bricks having no or very little quantity of plastic polymer took longer before getting soaked with water, they still were very permeable due to weak forces that held together the

grains of the laterite soil. Also, the permeability of the bricks was greatly enhanced upon increasing the amount of plastic polymer additives, the polymer grains having an approximate size of 1-2mm in diameter banded poorly with the laterite grains bonds of which could easily be broken by the absorption of water. Factors resulting in the collapse of Laterite bricks are;

- Absence of binder in the mixture
- Presence pores caused by organic matter burnt off during the heating process.
- Poor bonding between the laterite grains and polymer granules.
- Presence of cracks in bricks having a higher percentage of polymer

The bricks having a higher percentage of plastic polymer were observed to soak up and crumble after few minutes of immersion in water. The properties of the laterite soil used in the production of the bricks also influenced the permeability the bricks. These properties include engineering properties like sieve analysis, liquid limit and plastic limit.

#### IV. Conclusion

The brick samples used for this research were oven dried for 24 hours at a temperature of 105°C. The conclusions from the aforementioned experiments are as follows. The Compressive Strength tests carried out showed that the compressive strength of oven dried Laterite brick is inversely proportional to the containing quantity of polypropylene fiber. It was also observed from the experiments conducted that the strength of Laterite bricks is affected greatly by the amount of polymer fiber it contains.

Results from this research also showed that in order to maintain the structural capacity of oven dried Laterite bricks, the maximum amount of replacement with polymers should not exceed 5% of its total weight. Also, to maintain good engineering and mechanical qualities, the particle size of polymer granules or other similar additives should not exceed 1mm. Experiments tests gave a maximum compressive strength of 2.01N/mm<sup>2</sup> and according to BS3921, the compressive strength for a single storey building should be within the range of 1 to 5N/mm<sup>2</sup> which is also recommended by building authorities. The compressive strength of the oven dried Laterite bricks was observed to seriously decline when the amount of polymer additives exceeds 5%. These results show the inability of oven dried Laterite bricks to be used for high strength applications. However, the overall dead load of the building is greatly reduced due to the relatively low density and weight of the bricks. Thus, the bricks can be used for interior purposes, wall partitions and decorations the maximum flexural strength of 4.23N/mm<sup>2</sup> was recorded for the oven dried Laterite bricks. Similar to the compressive strength, the flexural strength of oven dried Laterite bricks is inversely proportional to the containing amount of polymer.

To maintain the flexural capacity of oven dried Laterite bricks, the used ratio of plastic in the brick material should not exceed 5% of the material weight.

The collapse of oven dried Laterite bricks and entire shrinking was observed to increase upon increasing the quantity of polymer additive. The greatest shrinkage of 4.25% for 15% polymer replacement was recorded during this research. The shrinkage of oven dried Laterite bricks showed a slight decrease as the amount was increased from 0% to 5% and begin to increase as the amount of containing polymer exceeded 5% of the total weight. Thus, the acceptable limit of shrinkage due to oven drying can be ensured by limiting the quantity of polymer or other similar materials to 5% of the material weight.

The weight loss by the oven dried Laterite bricks decreased upon a significant increase in the quantity of polymer additive. Although bricks of 15% polymer replacement had the least weight loss (1.16%), all brick samples satisfied the recommended maximum weight loss of 15% as stated in the British Standard BS5628.

This research shows that oven dried Laterite bricks failed totally when undergoing the test of water absorbing quality. As a result, oven dried Laterite bricks are not suitable for use in external purposes or in water logged areas or conditions but can be used for internal walls, partitions and for other internal structural purposes.

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O.A.Saliu. "Analysis Of The Effect Of Polypropylene Polymer(Crushed Plastic Waste)On Oven Dried Laterite Bricks." *IOSR Journal of Mechanical and Civil Engineering (IOSR-JMCE)*, 17(6), 2020, pp. 45-53.